THE CANADIAN INTENSE NEUTRON-GENERATOR

by

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The proposed Intense Neutron-Generator¹ is a multipurpose facility. It would produce intense beams of thermal neutrons for solid-state and low-energy nuclear physics studies and provide irradiation facilities for advanced research in nuclear chemistry, in materials science and for production of radioisotopes of research and commercial value. It would also provide copious sources of mesons and energetic nucleons for intermediate-energy nuclear-structure studies.

The primary neutron source, $\sim 10^{19} \text{ sec}^{-1}$, **42** ould be generated by bombarding a lead-bismuth target with a continuous 65 mA beam of 1 GeV protons. The same beam, and at a later stage of development, an auxiliary H⁻ beam, would be used simultaneously for producing secondary beams of π - and μ -mesons and energetic nucleons.

The overall plan, shown in Fig. 1, divides naturally into linear accelerator and beam-applications areas. The latter area, shown in more detail in Fig. 2, was planned to be easily modified and extended. The basic system includes a thin meson target traversed by the full 65 mA beam and, at the end of the transport system, the thermal-neutron target which absorbs the full beam. Subsequent elaborations would provide a split-beam channel for H⁻ ions co-accelerated with the protons, and for other secondary beam channels into which part or all of the main beam may be diverted. Ample space is allowed for adding a second transmission meson target, more experimental floor area, extra shielding if needed, and possible future facilities, for example, a storage ring. All beams are enclosed in tunnels shielded by about 8 metres of sand.

The thermal-neutron target area is shown in more detail in Fig. 3. The proton beam enters the building near ground level, is bent upward and then vertically downward into the liquid lead-bismuth target. The latter, a circulating, cooled, eutectic mixture, is surrounded by a tank of heavy-water moderator to yield a flux of 10^{16} cm⁻² sec⁻¹. Beam tubes and isotope irradiation facilities would be placed within and around the heavy water.

Fluxes near 10^{16} cm⁻² sec⁻¹ are difficult to obtain

with fission reactors because of core heating and fuel consumption limitations. The spallation-evaporation process by 1 GeV protons has several advantages, notably liberating about 4 times less heat in the primary source per output neutron.* About 20 neutrons per proton are expected⁴. Only 39 of the 65 MW beam power appears in the liquid metal; the remainder is radiated by nuclear processes to the heavy-water and surrounding shield.

The transmission meson target will probably be a falling curtain of liquid lithium, 0.1 gm/cm^2 thick. It would remove 0.2% of the main beam and have to dissipate about 15 kW of heat.

A Separated-Orbit Cyclotron to produce the proton beam was seriously considered¹. However we have now chosen a linear machine, adapted from the design of the Los Alamos Meson Physics Facility⁵ for 100% duty factor, for detailed study. Improved accelerating structures developed at Los Alamos⁶ and advances in crossed-field microwave generators⁷ influenced this choice.

Figure 4 and Table I illustrate the current design concept and main parameters of the machine. The injection system is a D.C. Duoplasmatron ion-source delivering 120 mA of positive ions, about 70% protons, accelerated to 0.75 MeV in a Pierce geometry column. With a double-drift-space harmonic buncher we expect 85% capture efficiency into the linac. A drift-tube structure consisting of 9 tanks and operating at $268\frac{1}{3}$ MHz accelerates the beam to 106 MeV. The first tank will be a $2\beta\lambda$ structure to ease quadrupole design problems in containing the transverse space-charge defocusing. At 106 MeV a transition is made to a coupled-cavity accelerator operating at 805 MHz consisting of 322 tanks driven in pairs by 0.5 MW RF generators. The 3:1 frequency ratio is dictated by a desire to be capable of simultaneously accelerating about 1 mA of negative hydrogen ions with the 65 mA of protons. The negative ions could be easily separated from the protons by an analysing magnet at the out

The design concept of the radiofrequency generators is shown in fig. 5. While the crossed-field device used as an output stage has low gain it is responsible for most of the DC to RF conversion; an efficiency of 85% is believed achievable and indeed has been accomplished in magnetrons⁸. With this we expect to approach an A.C. line power to beam power efficiency of 50%.

Our current programme includes studies of particle dynamics and beam stability in the machine, development and testing of ion sources and experimental radiofrequency tubes,

^{*}This scheme for producing neutrons in large quantities is not new; an extensive development program, the MTA project, was pursued in the USA in the early 1950's². Lewis³ discussed potentialities in 1952.

and design and testing of accelerator structures. We propose to construct an experimental injection system and first drift-tube tank to accelerate a 65 mA beam to 5 MeV and verify the beam behaviour in the beginning of the machine. We also propose to construct a short section of the main coupled-cavity accelerator as a prototype engineering and systems test. The section will be loaded with 65 mA of electrons and accelerate them to 6 MeV.

The Science Council of Canada was asked to review our proposals and has reported favourably. So far funding has permitted only a study with limited experimental work.

If the project is approved in the near future completion of the first phase by 1974 at a cost of about \$130M U.S. is envisaged. Other facilities could be added during the following 5 years.

Acknowledgments

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DISCUSSION (condensed and reworded)

J.P. Blewett (Brookhaven): Could you clarify what you meant by the first phase?

<u>Tunnicliffe:</u> This would consist of the main thermal neutron target, one transmission meson producing target and a relatively small experimental area.

J.M. Peterson (LRL): Why do you prefer to accelerate negative ions, i.e., H , in preference to splitting the proton beam?

<u>Tunnicliffe</u>: We have come to the conclusion that the present state of the art in fast beam switching systems would not allow us to split the beam with a tolerable beam loss. However the negative ion beam is quite easily separated.

K.H. Reich (CERN): You discussed the use of a different design for the first tank. Have you compared this with the use of a higher energy pre-accelerator?

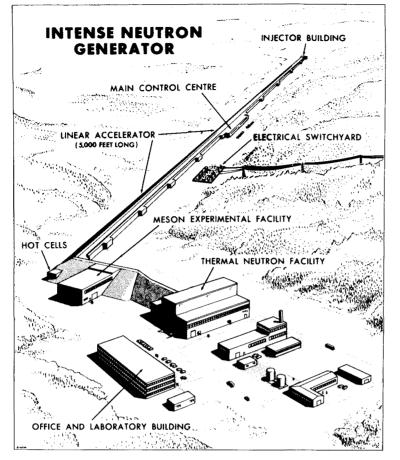
<u>Tunnicliffe</u>: Yes, this appears to be a compromise between reliability and complexity of tank design.

TABLE I

				· · · ·
Linear Accelerator Design Parameters		Waveguide Section		
Output energy " spread	1000 MeV \sim ± 3 MeV	Injection energy 106 MeV		
-	$\sim \pm 3$ MeV 65 mA	Output energy 1000 MeV		
Output current, positive ions	65 mA	Operating frequency 805 MHz		
(basic machine)		Length 1430 metres		
negative ions	\sim 0.5 mA	Number of tanks 322		
(full machine)		Average energy ga	in/tank 2.8 MeV	7
Length	1540 m.	tank length	3.4 met	res
Injection (basic machine)		tank diameter 28 cms. beam hole diameter 3.8 cms.		
type	Duoplasmatron	beam hole diameter power/tank		
Positive ion source cype current	120 mA (70% protons)			0.25 MW
D.C. accelerating voltage	750 kV	cosq	0.9 \sim 1 metre 1 quadrupole triplet/tank interspace quadrupole gradient - 3 kg/cm	
Buncher (double-drift harmonic	34 kV fundamental	Tank spacing		
type)	15 kV 2nd harmonic	Focusing		
-1 /	0.78 metre drift space			
Capture efficiency into linac	86%	R.F. generators 0.5 MW (one/2 tanks)		(one/2 tanks)
capture criticities into finde	00/3	Total R.F. power	80.5 MW	
Alvarez Section		Total R.F. losses	22.4 MV	1
Injection energy	750 keV	Shielding & Activation		
Output energy	106 MeV	Shielding & Accivacion	Maximum beam spill	
Operating frequency	268.3 MHz		allowing reasonable	
Length	110 metres	Proton Energy	access 10 hours	Shielding thickness
Input admittance invariant	7.6 π mm. mrad.	MeV	after shutdown	metres of sand
Input energy spread	± 15 keV max.	Mev	arter shutdown	
Number of tanks	9	10	500 nA/metre	2.3
Tank l	2 $\rho\lambda$ design, length 6 metres	50	50	5.0
	Energy gain 4 MeV	200	10	7.6
	Quadrupole magnets in every	1000	2	8.0
	drift tube, gradients 5 to 2 kg/cm,	R.F. Power Supplies		
	$\cos \varphi_s = 0.82$		(m	-field reentrant-beam
Tanks 2-9	$ ho\lambda$ design, length \sim 12 metres Guadrupole magnets in alternate	Main power amplifiers	devices (e.g. Amplitrons)	
	drift tubes, gradients 4 to 2 kg/cm	Driver amplifiers	Klystro	
	in tank 2, others 1 kg/cm, $\cos\varphi_e = 0.9$	D.C. power supplies	18 MW m	
		Objective A.C. to R.F	. conversion efficience	Y 80%
Tank diameter	\sim 70 cms.			
Drift tube diameter	\sim 12 cms.			
Drift tube bore	1.5 to 3.0 cms.			
Tank separation $(2\beta\lambda)$	22 to 82 cms.			
R.F. power requirements (approx.)	0.4 MW tank 1			
(beam + loss)	1.2 MW tanks 2-9			
R.F. generators	1.2 MW/unit (one/tank)			
	(tank 1 - special) 10.0 MW			
Total R.F. power	3.5 MW			
Total R.F. losses	5.5 MM			

TABLE I (continued)

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Perspective View of ING Project

Figure 1

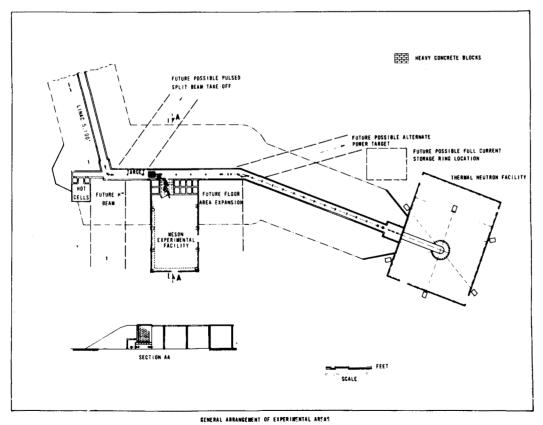
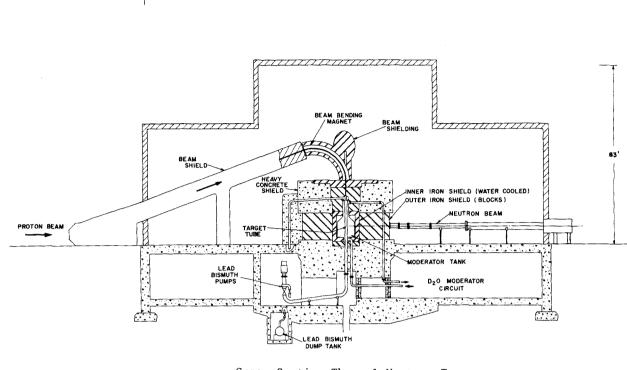
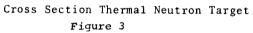


Figure 2





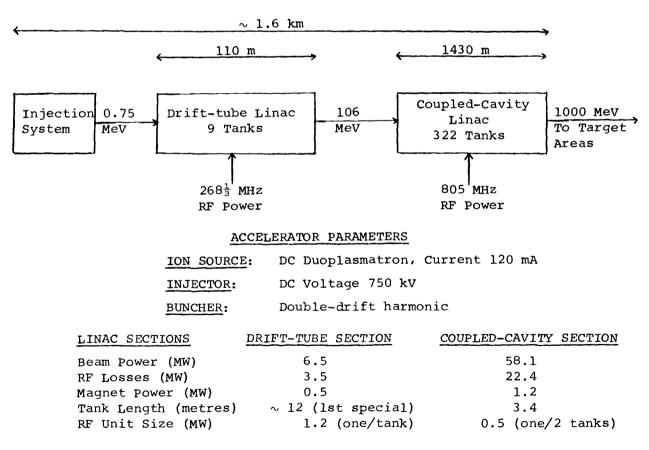


Figure 4

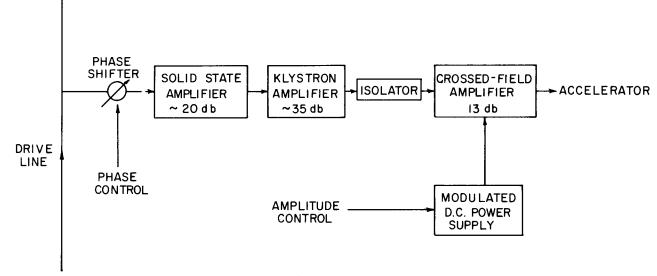


Figure 5