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Large plastic scintillator panels with WLS fiber readout: Optimization of components



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ABSTRACT

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Keywords: Plastic scintillator Photomultiplier tube Wavelength shifting fiber Photoelectron Results are presented on R&D efforts to design and build large size veto panels, optimized for underground low background experiments, in the most efficient and economical way using commercially available components. A variety of plastic scintillators, photomultiplier tubes, wavelength shifting fibers, and light reflector combinations were tested. Results of these studies and performance of a 2.2 m long panel are presented. © 2014 Elsevier B.V. All rights reserved.

1. Introduction

Highly efficient and compact veto systems to tag cosmic muons become increasingly important components for low background experiments, such as searching for Dark Matter and Double Beta decay [1–4]. Requirements for such a system are compactness, hermiticity, very high efficiency for muon identification and immunity from ambient gamma ray background. Often such a system has to operate in a limited space so that large lifting fixtures to mount the system are not always an option.

Natural radioactivity present for deep underground experiments consists primarily of gamma rays from decay of U and Th series and ⁴⁰K in surrounding materials. Such gammas are normally filtered out by passive shielding surrounding the low background detector. However, these gammas can result in large event rates in the veto system and therefore significant dead time if gamma and muon signals are not properly separated. The most straightforward way to achieve good separation between gammas and muons is the use of thick scintillator [5]. For scintillator with 5.10 cm thickness a muon deposits about 10 MeV of energy which is typically three times the energy of ambient gammas. Limited or non-uniform light collection can smear responses from both gammas and muons in a veto system which is usually located outside of gamma shielding. However, the large difference in initial energy deposition provides a suitable safety margin. This is extremely important especially for deep underground

experiments where the ratio of gamma to muon events is of the order of $10^7 - 10^9$.

As the price of plastic scintillator (PS) is a significant factor in total detector cost it is tempting to reduce scintillator thickness. Moving from 5.10 cm to 2.54 cm scintillator is a challenge because energy depositions from muons and energetic gammas are close to each other thus increasing the chance of misidentification. To achieve high efficiency for muons while maintaining good discrimination from gammas, excellent uniformity and relatively large light collection are required. In addition to having much lower cost, 2.54 cm veto panels are lighter and easier to handle. For example the Majorana Demonstrator (MJD) [6] is planning to use large area veto panels with dimensions up to 1.3 by 1.7 m². The weight of such a panel built with 5.10 cm scintillator is \approx 150 kg and requires special lifting fixtures for installation. Since the final Majorana Demonstrator is housed in a location with limited space, moving such a panel around becomes a nontrivial problem. On the other hand an identical panel built out of 2.54 cm scintillator is manageable, and can be moved by hand. Our R&D effort was to establish the feasibility of constructing veto panels using 2.54 cm scintillator while maintaining good discrimination between muons and gammas. To avoid bulky light guides we chose to read out light from scintillators with wavelength shifting (WLS) fibers. Systems with similar arrangements have been studied extensively primarily for accelerator based experiments [7–11]. However implementation of this technology for underground experiments raises significant challenges, as the absence of timing signals from the accelerator and/or information from multiple tracking layers complicates the discrimination of minimum ionizing signals from ambient background.

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2. Experimental apparatus

To collect light from the scintillator we chose to use WLS fibers running along the scintillator in shallow grooves. An overall view of one panel with fibers and photomultiplier tube (PMT) is shown in Fig. 1. To optimize the proposed design the R&D program evaluated components to select the most cost efficient combination. Five scintillators, five wavelength shifting fibers, two PMT models, and a variety of wrapping materials were tested. See Table 1.

BC-404 and BC-408 are plastic scintillators from SAINT-GOBAIN CRYSTALS. Important properties for BC-404 are the following: light output relative to anthracene is 68%, wavelength of maximum emission is 408 nm and light attenuation length is 140 cm. The corresponding parameters for BC-408 are light output 64%, wavelength of maximum emission 425 nm and light attenuation length 210 cm. EJ-204A and EJ-204B are products of ELJEN TECHNOLOGY. They have similar properties to BC-404 but at a lower cost. UPS-923A is plastic scintillator from Kharkov Crystal Institute (Ukraine). The latter scintillator has been used for the GERDA [12] veto system. All test scintillator panels had dimensions 50.0 cm \times 20.0 cm \times 2.54 cm except UPS-923A which had thickness 3.0 cm.

The PMTs studied were HAMAMATSU photomultipliers from the R9880U series: R9880U-20 and R9880U-210 (two samples each). Both types have the same dimensions: height 12 mm, diameter 16 mm with effective photocathode diameter 8 mm. Photocathode material for R9880U-20 is multialkali and for R9880U-210 ultra bialkali (UBA). Both are constructed with 10 dynode stages which allow typical gain 2×10^6 at 1000 V.

WLS fibers Y-11(150), Y-11(200), Y-11(300) from Kuraray and BCF-91A. BCF-92 from SAINT-GOBAIN CRYSTALS were employed. Y-11 fiber has diameter 1 mm and multi-cladding structure. BCF-91A and BCF-92 fibers have diameter 1 mm and single cladding structure. For Kuraray fibers the numbers in parentheses indicate dye concentrations in ppm.

The last column lists reflector (REFL) materials studied. TYVEK-1025D, TYVEK-1056D and TYVEK HomeWrap are superbonded olefin products from DuPont Company with good opacity and whiteness and are in common use as reflector material for panels. TYVEK-1025D has thickness 5 mil and mass density 1.25 oz/yd² while TYVEK-1056D has thickness 6.3 mil and mass density 1.60 oz/yd^2 (units are taken from Data Sheets). They are used primarily in the printing industry. TYVEK HomeWrap is used in the home building industry. It has density 1.80 oz/yd^2 and is somewhat less expensive. VM2000 and ESR (Enhanced Specular Reflector) are products from the 3M Company and are designed to ensure high reflectivity.

The WLS fibers rested in 3 mm deep and 1 mm wide U shaped grooves cut in the scintillator by a circular saw. Only straight line grooves were cut. At the end distant from the PMT, the fibers exited the scintillator and reentered in an alternate groove. For the measurements an air gap between scintillator and WLS fibers was

Test scintillator (50 cm x 20 cm x 2.54 cm)



Fig. 1. Test panel.

Table 1
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N	/laterials	studied.

PS	PMT	WLS	REFL
BC-404 BC-408 EJ-204A EJ-204B UPS-923A	R9880U-20 R9880U-210	Y-11(150) Y-11(200) Y-11(300) BCF-91A BCF-92	TYVEK-1025D TYVEK-1056D TYVEK HomeWrap VM2000 ESR Aluminum foil Aluminized mylar film



Fig. 2. Single photoelectron spectrum: the dashed blue line is fit by a Gaussian distribution for pedestal (parameters Ampl1, Mean1, Sigma1), and the dashed red line is fit by a Gaussian distribution to the single photoelectron peak (parameters Ampl2, Mean2, Sigma2), (For interpretation of the references to color in this figure caption, the reader is referred to the web version of this paper.)

employed and no optical grease was used. Extensive studies were conducted to learn how to cut grooves in the scintillator so that extra polishing was not required. Parameters such as saw rotation rate, scintillator feed rate and cooling water flow rates were varied until it was possible to achieve grooves with a suitably polished surface in only two passes of the saw. The quality of the groove surfaces was evaluated by visual inspection. The WLS fibers were looped in alternate grooves and the ends were coupled using optical grease to a PMT secured in a special holder. See Fig. 1. A light tight box was constructed for the test measurements. Data were recorded using a LabView 8.6.1 based DAQ system. A FAST CAMAC 16 channel charge integrating ADC Module (QADC) was used to measure signal charge with integration gate 200 ns.

3. Test of components

3.1. PMT test

For direct comparison of the combinations tested it is useful to express light yield in terms of number of photoelectrons. For each test panel, gain vs. high voltage was calibrated and the position of the single photoelectron peak is determined. The single photoelectron signal was identified using a pulsed LED (blue light) with average intensity 0.01 photoelectrons per pulse. Fig. 2 shows the single photoelectron peak position for a typical test panel at 920 V. The total systematic error in conversion into Phe. units is estimated to be about 15% based on the accuracy of single Phe. and gain measurements.

For gain calibration the LED intensity was increased to about 10 Phe. per pulse as the average muon signal is considerably larger than the single photoelectron one. An external generator was used to trigger the DAQ and generate short LED pulses (\leq 50 ns). The results of this calibration are shown in Fig. 3 for two typical PMTs, one from series R9880U-210 (red line) and one from series R9880U-20 (blue line).

Two types of PMT, R9880U-20 and R9880U-210, were investigated. Measurements of muon spectra showed similar performance with respect to gain, single Phe. spectrum, and overall quantum efficiency for WLS emission spectra.

3.2. Measurement of attenuation in WLS fibers using muon spectrum

To compare attenuation properties of different WLS fibers the cosmic ray muon peak was used. For the measurements extra long WLS fibers were used to increase the distance between the PMT and the edge of the scintillator panel. In Fig. 4 the dependence of the muon peak position amplitude vs. the distance between the PMT and the edge of the PS is presented for Y-11(200) and for BCF-91A fibers. For the measurements BC-408, a single Y-11(200) or BCF-91A WLS fiber and REFL material TYVEK-1025D were employed. Due to the limited space in the light tight box it was necessary to bend WLS fibers longer than 95 cm which resulted in light reduction of 2% (measured in special runs). The bending radius was approximately 20 cm. Correction for this effect is



Fig. 3. Gain vs HV dependence: the red line is for the PMT R9880U-210 series, and the blue line for R9880U-20 series. (For interpretation of the references to color in this figure caption, the reader is referred to the web version of this paper.)



Fig. 4. Attenuation for Y-11(200) (red dots) and BCF-91A (blue dots) WLS fibers. Attenuation length is in centimeters. (For interpretation of the references to color in this figure caption, the reader is referred to the web version of this paper.)

included in the experimental data. Experimentally the response can be fit by the sum of exponential functions. The light output of a fiber is parameterized by

$$I(x) = I_{0S} \exp\left(-\frac{x}{\lambda_1}\right) + I_{0L} \exp\left(-\frac{x}{\lambda_2}\right)$$
(1)

where λ_1 is the short attenuation length, λ_2 is the long attenuation length and $I_{0T} = I_{0S} + I_{0L}$ is the total light yield. Fig. 4 shows normalized experimental data for the light output of the Y-11 (200) (red dots) and BCF-91A (blue dots). The attenuation data are well fit by Eq. (1) with attenuation lengths $\lambda_1 = (20 \pm 10)$ cm and $\lambda_2 = (745 \pm 124)$ cm for Y-11(200) fiber and with $\lambda_1 = (25 \pm 11)$ cm, and $\lambda_2 = (442 \pm 113)$ cm for BCF-91A fiber.

Similar results have been previously reported. For example the NOVA collaboration [13] conducted extensive studies of the transparency of Y11 fibers vs. wavelength. They measured an attenuation length of \approx 6–8 m at wavelength \approx 520 nm near the second maximum of emission for K27 dye (the major component of Y11 fiber). They conclude that attenuation does not depend appreciably on dye concentration but is determined by core polystyrene attenuation. We did not measure attenuation of Y11 fibers with a different dye concentration. The MINOS collaboration [14] found that while both Kyraray (Y11) and Bicron BCF91-A fibers were acceptable for their purposes, measurements indicated a longer attenuation length for Y11 (Fig. 5.10 in Ref. [14]) than for BCF91-A. After visual inspection of both Y11 and BCF-91A samples provided to us for tests we observe less uniformity in BCF-91A fiber.

3.3. Light yield with different numbers of WLS fibers

Adjacent grooves in the test panel plastic scintillator are separated by 2.84 cm. Fibers are placed in one groove and looped to return in an alternate groove. Each test panel contains six grooves (three loops, see Fig. 1). The response, when loops are added, is shown in Fig. 5, where results are presented for a BC-408 panel with WLS fiber Y-11(150) coupled to a R9880U-20 PMT at 950 V. As expected the addition of fiber loops can be used to increase light collection.

3.4. Light yield for various reflectors

The dependence of light yield on wrapping materials was also investigated. For these measurements PS BC-408 with WLS fiber Y-11(200) coupled with PMT R9880U-20 at 950 V was used. For the three types of TYVEK (1025D, 1056D and HomeWrap) reflectors at least two layers of material were necessary to prevent the



Fig. 5. Light yield as a function of the number of WLS fiber loops. The red line is a linear fit to experimental data. (For interpretation of the references to color in this figure caption, the reader is referred to the web version of this paper.)

Table 2

Light yield (in Phe.) at muon peak for different reflectors.

Tyvek-1025D	Tyvek-1056D	Tyvek HomeWrap	VM2000	ESR	Aluminum foil	Mylar film
165.8 ± 0.4	173.4 ± 0.1	194.8 ± 0.2	260.3 ± 0.3	246.7 ± 0.6	104.7 ± 0.3	64.3 ± 0.1



Fig. 6. Spectrum for PS BC-404. The dashed blue line is a fit by an exponential distribution for environmental gammas (parameters Const1, Slope), and the dashed red line is the Landau distribution for muons [parameters Const2, MPV (most probable value), Sigma]. (For interpretation of the references to color in this figure caption, the reader is referred to the web version of this paper.)

escape of light. Addition of a third layer of TYVEK increased light yield by less than 10%. For reflectors VM2000, ESR and Aluminum Foil a single layer was used. Five layers of aluminized Mylar Film were also tested as reflector material. As shown in Table 2 significant improvement of light yield is observed with VM2000 and ESR. With these reflectors up to 45 Phe./MeV were collected. VM2000 is no longer available from 3M and has been replaced by ESR which 3M Company suggested had slightly improved reflectivity although our measurements do not confirm this for our application.

4. Results of measurements

4.1. Measurements on test panels

All PS-PMT-WLS combinations listed in Table 1 were tested. Each was wrapped individually with reflective material. Fig. 6 shows a typical charge spectrum in single Phe. units for BC-404 measured in the test laboratory at the Science and Engineering Research Facility (University of Tennessee, Knoxville, TN, USA). The measurement was done with WLS fiber Y-11(200) wrapped in REFL material TYVEK-1025D and PMT R9880U-20 (applied voltage 950 V). The background gamma flux is shown as a dashed blue line and is fit to a single exponential function. It is mainly due to the 2.615 MeV gamma line from ²⁰⁸Tl, a product of the ²³²Th decay chain. The muon peak is fit by a Landau distribution, shown as the dashed red line.

A convenient parameter for evaluation of gamma/muon discrimination is the peak to valley ratio (P/V). As can be seen in Fig. 6 a larger value of this ratio represents improved separation of the gamma and muon spectra resulting in greater muon efficiency and reduced false gamma triggers. The peak to valley ratio for the combination BC404/Y11(200), shown in Fig. 6, is 4.9.

4.2. Light yield studies

Measurements were conducted on test panels constructed from combinations of the five PS materials and five WLS fibers

Table 3						
ight yield dependence	(in Phe.)) for PS	WLS :	fiber	combinatio	ons.

PS	Y-11(150)	Y-11(200)	Y-11(300)	BCF-91A	BCF-92
BC-404 BC-408 EJ-204A EJ-204B UPS-923A	$\begin{array}{c} 121.7\pm0.4\\ 130.1\pm0.2\\ 99.5\pm0.4\\ 100.4\pm0.4\\ 54.8\pm0.2 \end{array}$	$\begin{array}{c} 167.4 \pm 0.2 \\ 165.8 \pm 0.3 \\ 131.7 \pm 0.3 \\ 133.1 \pm 0.1 \\ 72.2 \pm 0.2 \end{array}$	$\begin{array}{c} 160.9\pm0.2\\ 165.4\pm0.3\\ 127.3\pm0.2\\ 129.4\pm0.3\\ 74.5\pm0.1 \end{array}$	$\begin{array}{c} 114.9\pm0.2\\ 119.5\pm0.2\\ 92.6\pm0.2\\ 94.8\pm0.1\\ 52.3\pm0.1 \end{array}$	$\begin{array}{c} 78.8 \pm 0.2 \\ 80.5 \pm 0.2 \\ 64.6 \pm 0.1 \\ 63.5 \pm 0.2 \\ 34.4 \pm 0.1 \end{array}$

listed in Table 1. Each PS was wrapped with two layers of TYVEK-1025D reflector. No optical grease was used between PS and WLS fibers. A series R9880U-20 PMT at 950 V was employed in all measurements. Light yield (in Phe.) at the muon peak for various combinations of scintillators and fibers is shown in Table 3. For each scintillator the light yield varies from worst case (BCF-92) to the best one (Y-11(200)) and Y-11(300)) by approximately a factor of two.

Table 3 demonstrates superior light yields from plastic scintillators BC-404 and BC-408 and WLS fibers Y-11(200) and Y-11 (300). GEANT-3 [15] simulation predicts most probable energy deposition by muons in 2.54 cm scintillator to be 5.5 MeV, indicating that the better combinations, e.g. BC404/Y11(200), provide an approximate sensitivity of 30 Phe./MeV. To assess the reliability of the connection procedures between fibers and the PMT a single BC408/Y11(200) test panel was disconnected and reconnected four times. The muon peak position was measured after each step and varied less than 1%. The errors quoted in Table 3 do not include possible contributions from this effect.

4.3. P/V ratio for different PS/WLS combinations

In Table 4 the P/V dependence on WLS fibers for different PS is shown. The numerical value of the ratio, of course, depends on ambient background conditions but for a given muon to gamma ratio a large value indicates better performance. The largest P/Vratios are for Y-11(200) and Y-11(300) WLS for nearly all scintillators. Comparison of Tables 3 and 4 demonstrates that higher P/Vvalues are heavily correlated with greater light yields at least for panels of the size tested. It is expected that the correlation will continue for larger panels but we have not specifically investigated this question.

5. Large panel test

The focus of our R&D was to determine optimal technology for construction of large veto panels for the Majorana Demonstrator [6]. An important requirement is reduction of dead areas to an absolute minimum to have a good geometrical efficiency for muons. To achieve this goal the PMT is located above the plane of scintillator. While a variety of panel lateral dimensions are required in the Demonstrator, a typical panel is 170 cm long and 80 cm wide with thickness 2.54 cm. To explore the properties of larger panels we constructed a panel with the dimensions of the longest panel required by the Majorana Demonstrator, which is shown in Fig. 7. Five fibers extend the full length of the panel and return through an alternate groove. The total number of grooves is 10. Fibers in the panel are bunched together at one

 Table 4

 P/V dependence on WLS fibers for different PS.

PS	Y-11(150)	Y-11(200)	Y-11(300)	BCF-91A	BCF-92
BC-404	4.5	4.9	4.7	4.1	3.2
BC-408	4.5	5.2	5.5	4.5	3.0
EJ-204A	3.4	4.3	4.6	3.5	2.7
EJ-204B	3.3	4.5	4.6	3.6	2.6
UPS-923A	2.7	3.4	3.5	2.5	1.8



Fig. 7. Veto panel $224\,\text{cm}\times33\,\text{cm}\times2.54\,\text{cm}$ in Aluminum box with muon telescope.



Fig. 8. Panel uniformity light collection. The blue line is a uniformly wrapped panel and the red line is with optimized two component wrapping. (For interpretation of the references to color in this figure caption, the reader is referred to the web version of this paper.)

end, bent upward with 6 cm radius and connected to the PMT. The scintillator plate is wrapped in reflective material and enclosed in a light tight Aluminum box (Al thickness = 1.59 mm). A single PMT was used in contrast to the widely employed system with PMTs attached to both ends of the fibers. This reduces the cost of electronics, PMTs, cables, etc. and ensures less dead space around veto panels. Wavelength shifting fibers ride freely in the scintillator grooves without optical coupling. Uniformity of response to muons was measured using a small movable scintillator telescope shown in Fig. 7 to select cosmic muons passing through the panel at specific locations.

Fig. 8 shows uniformity of light collection from the 224 cm long panel. Uniformity was measured by scanning along the panel with the muon telescope in steps of 20 cm. The vertical scale is the most probable light output for muons in photoelectrons. The horizontal scale is the distance from the end where the PMT is located. Blue points are the response of the panel with the scintillator wrapped uniformly with two layers of TYVEK-1025D. The fact that wrapping



Fig. 9. Self-triggering spectra by low threshold (red line) and high threshold (blue line). (For interpretation of the references to color in this figure caption, the reader is referred to the web version of this paper.)

materials have different light collection efficiencies can be used to improve panel response uniformity. Use of highly reflective material at the far end of panels with less reflective material near the PMT can significantly improve light collection uniformity. The effect of such optimized wrapping is shown in Fig. 8. Red points are the response of the panel with the scintillator wrapped in a combination of TYVEK-1025D and ESR reflectors optimized to improve uniformity. This non-uniform wrapping improved response uniformity (2.2% instead of 5.6%) and average light output increased. We have consistently noted for all of the larger panels constructed for MJD that light output is reduced from that observed in the small test panels. We are unable to fully account for this phenomenon but several factors seem to contribute, including wider spacing of grooves and longer WLS fiber lengths needed to reach the PMT.

In Fig. 9 the result of a run in self-triggering mode from the same panel is shown for two thresholds. The low threshold (red line) was chosen to detect all muons and consequently many ambient gammas. Clear separation is seen between muons and gammas. A higher threshold (blue line) retains 99% of muons but suppresses the gamma rate by a factor of 4. The trigger rate for gammas is then less than 10 Hz/panel which introduces negligible dead time into the system. For the trigger threshold we used an amplitude discriminator while light yield was determined by total charge. Due to the fast response of the PMT and the relatively large spread in arrival time of photons in a large scintillator, a low amplitude signal can correspond to a large total energy deposition. Therefore in Fig. 9 we do not observe a sharp energy cut.

6. Conclusions and discussions

A comprehensive study of combinations of various components used to build large veto panels is presented. It is demonstrated that with 2.54 cm scintillator and a single photomultiplier it is possible to achieve excellent light collection uniformity, large light output and good gamma to muon separation even for scintillation panels more than 2 m long. The best performance of panels for maximum light output and P/V ratio is the combination of (BC-408)+(Y-11(200))+(VM 2000). However, it is also the most expensive, and due to budgetary constraints we were not able to select this as a baseline for MJD. Of all components the most expensive is the scintillator which would account for 80% of the cost if BC-408 is selected. Since the prices quoted for the scintillators tested varied by nearly a factor of four, the scintillator choice was crucial and resulted in selection of EJ-204B even though the muon light yield was lower by 25–30%. Based on these considerations we selected a combination of EJ-204B scintillator, Y-11(200) WLS, optimized wrapping (ESR+TYVEK), and R9880U-210 PMT as a baseline for MJD. With this choice the use of 2.54 cm thick scintillator relative to 5.10 cm reduced the final cost of the MJD veto system by 60%.

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